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Draftsmen's Sketch Book for Parts for the Ford Motor Company

M. M.

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4 COMPANY *Ind Motor Co* SKETCH B'K *2236*
GEN. SUBJECT *42" & 32" Mills*
USED BY *M. M.* BEGINNING *10/26/23* COMPLETED

ORDER NO.	SUBJECT
<i>21109</i>	<i>32" BILLET MILL DRIVE</i>
<i>21109</i>	<i>32" Roll Housing</i>
<i>21008</i>	<i>42" Roll Housing</i>
<i>P 22</i>	<i>Weight 42" Roll</i>
<i>P 29</i>	<i>Supporting Pins</i>
	<i>Weights of 42 & 32 Drives</i>
	<i>Page 1.</i>

TO BE USED BY THE DRAFTSMAN FOR ALL SKETCHES, NOTES, CALCULATIONS AND DATA RELATING TO THE ABOVE COMPANY ONLY, UNDER NO CIRCUMSTANCES ARE LOOSE SHEETS OR PRIVATE NOTE BOOKS TO BE USED.

NO UNUSUAL EFFORT SHOULD BE MADE AT NICETY, BUT EACH ENTRY SHOULD INVARIABLY BE COMMENCED WITH THE SUBJECT AND DATE OF THE WORK, AND FULL NOTES MADE OF DATA ON WHICH CALCULATIONS ARE BASED AND THE RESULTS OBTAINED CLEARLY STATED.

BOOKS ARE TO BE ALWAYS QUICKLY AVAILABLE TO RECEIVE INSTRUCTIONS, SKETCHES AND DATA AS MAY BE GIVEN THE DRAFTSMAN AND HE WILL BE RESPONSIBLE FOR THEIR DELIVERY AT ANY TIME.

SUBJECT
COMPANY DATE

Approximate weight of
42" & 32" Mills

42" Mill

WORCESTER, MASS. Weight of bed, bearings
hoods & oil pans 25
Weight of shafts 18
Weight of gears 35

CO.

32" Mill

PROPERTY OF MORGAN CONSTRUCTION Weight of bed bearings
hoods & oil pans 150
Weight of shafts 33
Weight of gears 66

2 Weights
SUBJECT 42" Planing Mill
COMPANY Ford Motor Co DATE 11/2/23

B31885 Spur gear
B31895 Spur gear Spider

Bed Spur gear Half 30,155
" Bevel gear Half 47,550

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

W 3
SUBJECT 32" Billet Mill
COMPANY Ford DATE 11/2/23

30
48
78000
40

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

4
 SUBJECT 32" pipe, Hards
 COMPANY Gold Truck DATE 10/30/23

99.471 120.000 90.717 310.188	310.188 234 76.188	19 12 38 228 234	310.188 76.188 234
$76.188 \div 2 = 38.094$			
$234 \div 2 = 117$			
$79.576 \div 2 = 39.788$			

99.471 38.094 61.377	90.717 38.094 51.623	51.623 27.953 79.576
84.351 61.377 22.974	22.974 61.377 84.351	

23.75
99.69
21375
14250
21375
21375
23676375

23.75
0781
2375
19000
16625
1.854875
90.717
1.855
88.862

88.862
444310
533172
23.6760
177724
590360
533172
571980
533172
50708

WORCESTER, MASS.
CO.

PROPERTY OF MORGAN CONSTRUCTION

SUBJECT _____
 COMPANY _____ DATE _____

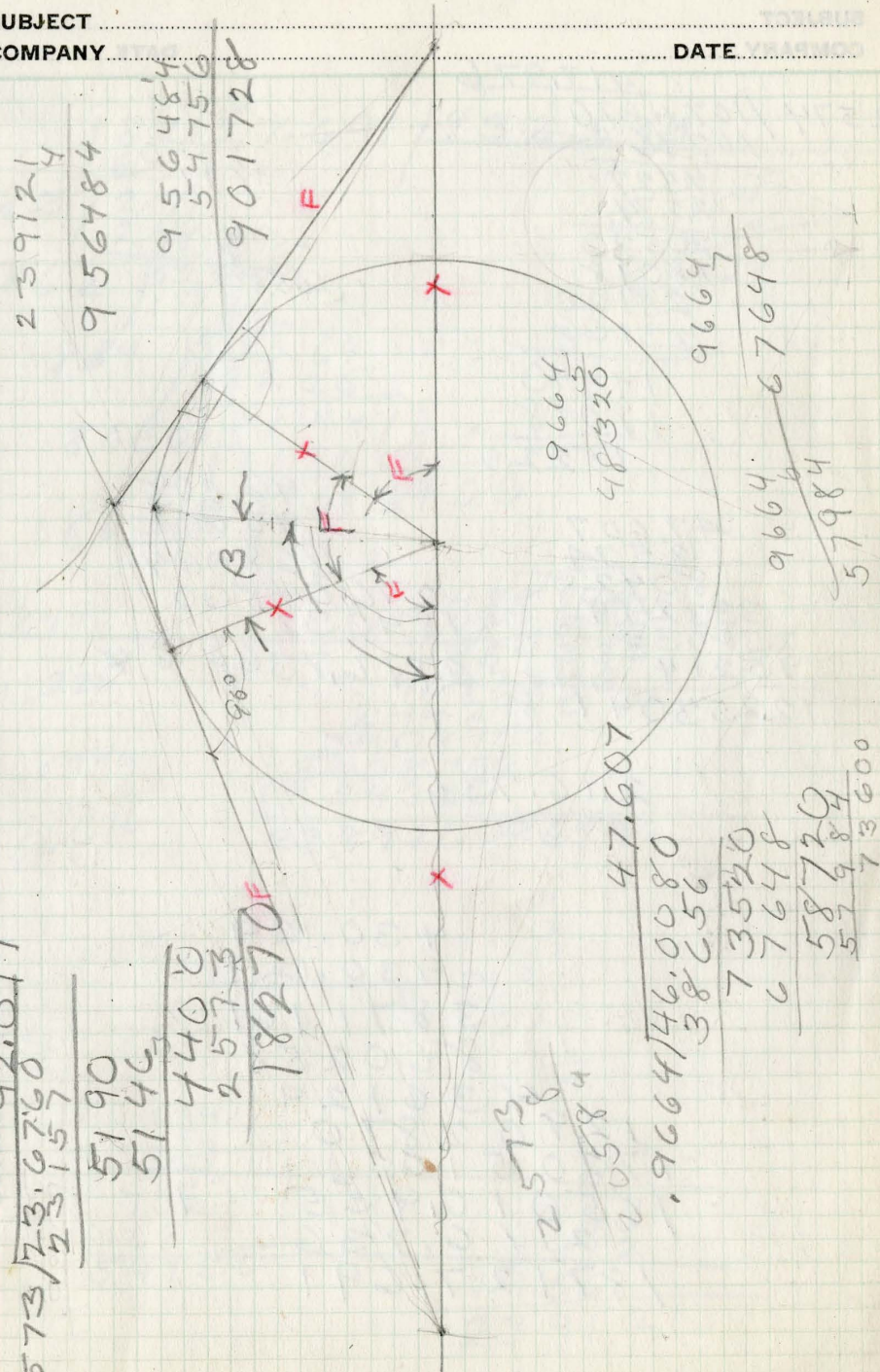
25730
23157

WORCESTER, MASS.
CO.

PROPERTY OF MORGAN CONSTRUCTION

239124
956484
956484
54756
901728

25730
23157
5190
5146
4400
25730
18270



25730
20584

9664
460080
38256
73520
67648
58720
57984
13600

9664
48320
9664
67648
57984
13600

SUBJECT

COMPANY

DATE

417.976
 2574 / 107.4870
 10296

4527
 2574
 20530
 18018
 25120
 23166

19540
 18018
 15220

47.607
 2574
 180428
 333249
 238035
 95214
 122530418

2116.736

430.129
 2430.129
 3871161
 2860258
 430129
 12903870
 1720516
 185010955
 2116.736
 187127.691

2574
 12870
 20582

46.008
 46.008
 368064

27604800
 184032
 2116.736064

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

SUBJECT

COMPANY

DATE

187127.691 / 432.594
 16

83 / 271
 249

862 / 2227
 17124

864 / 503.69
 42225

86509 / 814416
 778581

86518 / 3582900

865184

3460736

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

8445
 42225

8446
 6
 50676

86509

778581

234
 234
 936
 702
 468
 54756

488.594
 488.594
 21954336
 4397346
 2442970
 3908752
 3908752
 1954336
 238720.096796

19'-6"
 12
 38
 19
 228
 6
 234

489
 489
 4401
 3912
 1956
 239121

SUBJECT
 COMPANY DATE

238144 144 952576 54756 897820	489 418.113 70.887 5'-10.887"	417.976 3.9664 7671904 2507856 2507856 3761784 4039320064
--	--	---

897820/947.533 81 184/878 736	1887 13209
--	---------------

1887/14220 13209 18945/101100 94725 189503/637500 568509 68991	488 418.166 69.834	947 1894 18945 5 94725
--	--------------------------	------------------------------------

488 418.166 69.834 69 5'-9	417.976 3.9664 7671904 2507856 2507856 3761784 4039320064
--	---

WORCESTER, MASS.

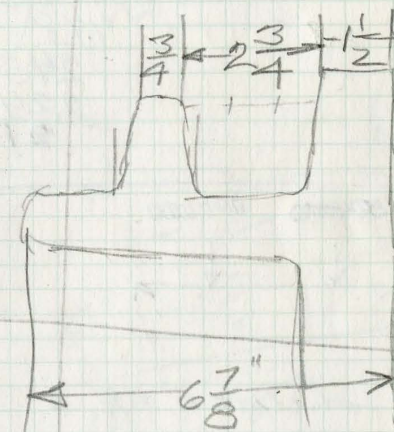
CO.

PROPERTY OF MORGAN CONSTRUCTION

SUBJECT
 COMPANY DATE

4173.766
14.234
488000

488



.875
2
2.625

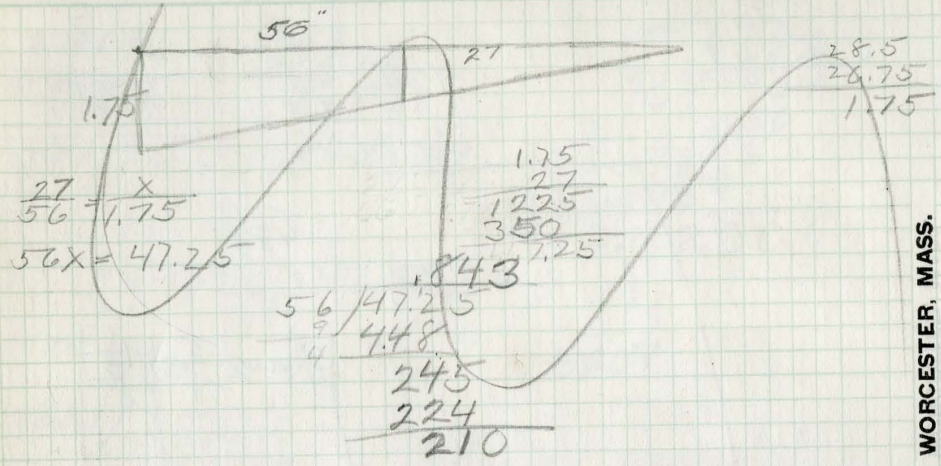
WORCESTER, MASS.

CO.

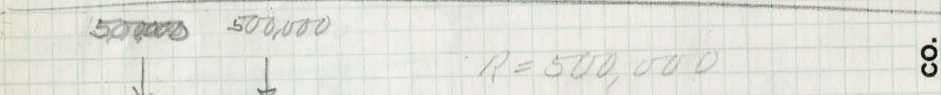
PROPERTY OF MORGAN CONSTRUCTION

10.

SUBJECT Spun Pipe Design (Intermediate Section)
 COMPANY Worcester, Mass. DATE 11/9/23



WORCESTER, MASS.



Max shear = $R_1 = R_2 = \frac{500,000}{10,000} = 50$ lbs/in

$M = \frac{(500,000)(2\frac{1}{2})}{4} = 1,250,000$ "lbs.

$\frac{1,250,000}{10,000} = 125$

$\frac{1}{6} = 125$

$312,000$

$125 = \frac{bh^2}{6}$

$750 = b \cdot 49$

$b = 15\frac{1}{2}$

$750 = b \cdot 81$

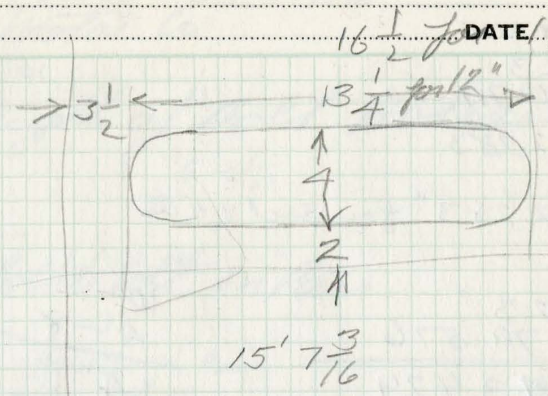
$9\frac{1}{2}$

PROPERTY OF MORGAN CONSTRUCTION

CO.

11

SUBJECT
 COMPANY DATE 11/9/23



$\frac{15}{12} = 30$

$500,000$

$1,250,000$

117.86

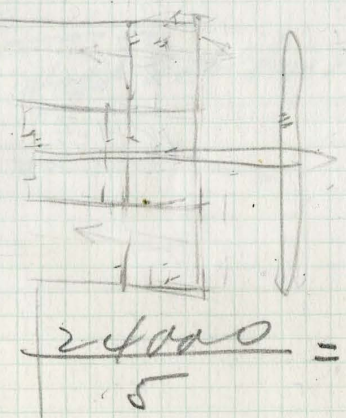
11310

$6 \cdot 3\frac{1}{8} = 476$

$5 \cdot 2\frac{3}{4} = 11\frac{1}{8}$

PROPERTY OF MORGAN CONSTRUCTION

CO.



$13\frac{1}{8}$

118

113

5

124

$\frac{24000}{5} = 4800$

12

SUBJECT _____
 COMPANY _____ DATE _____

$$\begin{array}{r} 123 \\ 90.717 \\ \hline \end{array}$$

32.283

32.283" for 3rd & 4th

$$\begin{array}{r} 123 \\ 79.576 \\ \hline 3.424 \end{array}$$
 $43\frac{1}{2}$ $32\frac{1}{4}$

$$\begin{array}{r} 10'-3 \\ 4'-8 \\ \hline 14'-11 \\ 2'-1\frac{3}{4} \\ \hline 12'-9\frac{1}{4} \end{array}$$

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

$$\begin{array}{r} 28.5 \\ 26.75 \\ \hline 1.75 \end{array}$$

1-

$$\begin{array}{r} 1.75 \times \\ 56 \times 34.75 \end{array}$$

$$56 \times = 60.8125 (1.086)$$

$$\begin{array}{r} 481 \\ 448 \\ \hline 332 \\ 336 \end{array}$$
 $5'-0\frac{1}{2}$ $15'-7\frac{3}{16}$ $13'-4\frac{15}{16}$ $2\frac{1}{4}$

$$\begin{array}{r} 26\frac{1}{4} \text{ difference} \\ 2 \\ \hline 13\frac{1}{8} \end{array}$$

12

10

 $25\frac{3}{4}$

$$\begin{array}{r} 10'-3 \\ 4'-8 \\ \hline \end{array}$$

$$\begin{array}{r} 14'-11 \\ 2'-1\frac{3}{4} \\ \hline \end{array}$$
 $12'-9\frac{1}{4}$

34.75

1.75

17375

24325

3475

608125

56

25

 $30\frac{1}{4}$

$$\begin{array}{r} 15'-7\frac{3}{16} \\ 2'-6\frac{1}{4} \\ \hline \end{array}$$

$$\begin{array}{r} 18'-1\frac{7}{16} \end{array}$$

SUBJECT

Oil Pans 32" Mill

COMPANY

Ford Motor Co.

DATE

12/13/23

Overall length of Bolt Holes 3rd Pair

 $19'-0"$ $6'-1\frac{1}{4}$ $12'-2\frac{1}{2}$ $31'-2\frac{1}{2}$ = Bolt to bolt on Pan $12'-9\frac{1}{4}$ for 3rd pair $18'-1\frac{7}{16}$ for 4th pair $30'-10\frac{11}{16}$ $30'-14.5$ $30'-10.6875$

2) 3.8125 = difference both ends

1.90625

 $= 1\frac{29}{32}$

PROPERTY OF MORGAN CONSTRUCTION

CO.

WORCESTER, MASS.

Overall length of Bolt Holes 1st & 2nd Pair

 $19'-0"$ $5'-0\frac{1}{8}$ $10'-0\frac{1}{4}$ $29'-0\frac{1}{4}$ = Bolt to Bolt on Pan $12'-9\frac{1}{4}$ for 3rd pair

SUBJECT
 COMPANY DATE

10'-3 2 6 1/4	15 12 30 15 180	56 25 3/4 30 1/4 8 1/4 18 126 152 1/4	18 1/2 126
12 9 1/4 1 1/2 1 1/8			
12'-11 1/8			194 1/8 155 1/8
155 1/8 152 1/4	14 13 42 14 182 18 1/8 11 1/8	15'-7 3/16 187 3/16 30 1/4 217 1/16 211 1/8	19 1/2 38 19 228
2 7/8			
56 3/4 25 3/4			56 9 65
30 1/4	211 1/8		
1		5 5/16 1 7/8	
187 3/16 30 1/4	228 65 293	7 3/16	
123 30 1/4		358 to nut and bolt.	
370 1/16 358	17 1/8	358 16 1/2	
12 11/16 3 3/4		374 1/2 = overall bolt dimension	
2/16 7/16 8 1/4			

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

SUBJECT
 COMPANY DATE

14 8 112 18 8 1/2 16 1/2 155 1/8 = overall for 163 Pair.	182 18 12/200 (1) 12 80	14 13 42 14 182 18 11 1/8 8 1/4	187 3/16 30 1/4 217 7/16 219 3/8 217 1/16 15 116
	18-3 3/8 12/219 3/8 12 99 96	219 3/8 155 1/8 374 1/2	
	182 18 1/8 8 1/4 208 1/4	219 3/8 18 1/8 11 1/8 208 1/4 11 1/8	182 18 11 1/8 12/211 1/8 (157 7/8) 91 84 7 1/8
	24 36 60-5' 500000	7-7 9 1/4 16 1/11	176 30 5280
	6'-3 1/8 5 1/2	15 1/7 1'-4 16 1/11	
	6' 8 5/8 10 3/4 8 5/8 2 1/8		2816 968 1600 300 4244
176 16 1056 176 2816	96 968 30 0		5280 968 160 300 6708
	8,000 480.00	480	

SUBJECT _____
 COMPANY _____ DATE _____

$\begin{array}{r} 10\frac{3}{4} \\ 1\frac{15}{16} \\ \hline 8\frac{13}{16} \end{array}$	$\begin{array}{r} 10.75 \\ 1.9375 \\ \hline 8.8125 \end{array}$	$\begin{array}{r} 15 \\ 12 \\ 30 \\ 17\frac{1}{2} \\ 3 \\ \hline 65 \end{array}$	<p>WORCESTER, MASS.</p>
$\begin{array}{r} 15\frac{3}{4} \\ 10\frac{3}{4} \\ \hline 25\frac{3}{4} \\ 187\frac{3}{16} \\ \hline 212\frac{15}{16} \end{array}$	$\begin{array}{r} 15 \\ 12 \\ 30 \\ 15 \\ \hline 180 \end{array}$	$\begin{array}{r} 3 \\ 21 \\ 22 \\ 29 \\ 65 \\ 18 \\ 56\frac{1}{4} \\ 8\frac{1}{4} \\ \hline 219\frac{1}{4} \end{array}$	
$\begin{array}{r} 58\frac{1}{4} \\ 14\frac{1}{4} \\ 14 \\ 14 \\ 14 \\ 18 \\ 13 \\ 13 \\ 13 \\ 13 \\ 29 \\ 11 \\ 11 \\ 21 \\ \hline 219\frac{1}{4} \end{array}$	$\begin{array}{r} 15\frac{3}{4} \\ 10\frac{3}{4} \\ 25\frac{3}{4} \\ \hline 217\frac{7}{16} \end{array}$	$\begin{array}{r} 13 \\ 5 \\ \hline 65 \end{array}$	<p>CO.</p>
$\begin{array}{r} 15\frac{3}{4} \\ 10\frac{3}{4} \\ 25\frac{3}{4} \\ \hline 30\frac{1}{4} \end{array}$	$\begin{array}{r} 15\frac{1}{2} \\ 26\frac{1}{4} \\ 18\frac{1}{2} \\ \hline 1630\frac{1}{4} \end{array}$	$\begin{array}{r} 18 \\ 12 \\ 36 \\ 17 \\ \hline 216 \end{array}$	
$\begin{array}{r} 153\frac{1}{4} \\ 155\frac{1}{8} \\ 153 \\ \hline 2\frac{1}{8} \end{array}$	$\begin{array}{r} 217\frac{7}{16} \\ 219\frac{1}{4} \\ \hline 217\frac{7}{16} \end{array}$	$\begin{array}{r} 31 \\ 65 \\ 18 \\ 12\frac{1}{8} \\ \hline 155\frac{1}{8} \end{array}$	<p>PROPERTY OF MORGAN CONSTRUCTION</p>

SUBJECT Weight of 32" oil Pan
 COMPANY 2nd Union DATE 12/21/23

length = 228"

$$\frac{48}{28} (76 \times 228 + 24 \times 228) \times (.28)$$

$$\frac{17300 + 5475}{22775} \text{ cubic in.}$$

$$\frac{22775}{.28} = 6,375 \quad 3\frac{1}{4} \text{ tons}$$

20 11.6875
 6.6428
5.0447

$\begin{array}{r} 198 \\ 2 \\ \hline 396 \end{array}$	$\begin{array}{r} 303 \\ 1189 \\ \hline 2200 \end{array}$	$\begin{array}{r} 3030 \end{array}$
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PROPERTY OF MORGAN CONSTRUCTION

SUBJECT

COMPANY

Solid Motor

DATE

dia shaft for worm drive

33,000

330,000 lbs.

660,000

3960,000 inches

$$P = 2\pi$$

$$d = \sqrt[3]{\frac{(321,000)(10)}{(3)(7500)}}$$

$$d = \sqrt[3]{\frac{3,210,000}{22,500}}$$

$$d = \sqrt[3]{14.3}$$

$$d = 2.5$$

$$\begin{array}{r} .9997 \\ .25 \\ \hline .9997 \\ .9997 \\ \hline .249925 \end{array}$$

$$\begin{array}{r} 2.676 \\ 1.338 \\ \hline 2.676 \end{array}$$

$$\begin{array}{r} 2.75 \\ 2.426 \\ \hline .324 \end{array}$$

$$\begin{array}{r} 3.00 \\ 3.24 \\ \hline 2.676 \end{array}$$

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

dia screw = 3"
 R. Mean Radius = 1.338
 a = angle of pitch =
 B = angle between flutes = 60°
 W = weight = 14,000 lbs
 φ = angle of friction = .25

$$\begin{array}{r} \tan \alpha = .0266 \\ \cos \alpha = .9997 \end{array} \quad \begin{array}{r} \tan \phi = .25 \end{array}$$

SUBJECT

COMPANY

DATE

$$F = \frac{WR}{a} \left(\frac{\tan \phi \cos a}{\cos \frac{\beta}{2}} + \tan \alpha \right)$$

$$F = \frac{(14,000)(1.338)}{8} \left(\frac{(.25)(.9997)}{.866} + \tan \alpha \right) \times .0266$$

$$F = \frac{(18700)}{8} \left(\frac{.2499}{.866} \times .0266 \right)$$

$$F = \frac{(18700)}{8} \left(.2885 \times .0266 \right)$$

$$F = (2337.5)(.0768)$$

$$P = 179,400$$

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

$$\begin{array}{r} 50'' \\ 4200 \overline{) 18000} \\ \underline{200} \end{array}$$

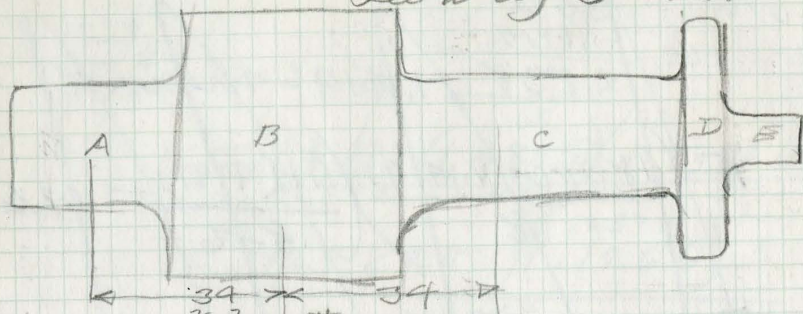
SUBJECT

COMPANY

Weight of 40" Roll

DATE

Lee Drug B 31891



$$\text{Weight of A} = 2590 \#$$

$$\text{Weight of B} = 15,500 \#$$

$$\text{Weight of C} = 3520$$

$$\text{Weight of D} = 2,280 \#$$

$$\text{Weight of E} = 917 \#$$

$$24,807$$

$$\text{Weight of A, Dia} = 21 \text{ length} = 26 \frac{3}{4}$$

$$\text{area} = 346.5$$

$$346.5 \times 26.75 \times .28 = 2590 \# = \text{Weight of A}$$

$$\text{Weight of C, Dia} = 21 \text{ length} = 36 \frac{1}{4}$$

$$346.5 \times 36 \frac{1}{4} \times .28 = 3520 \#$$

$$\text{Weight of B}$$

$$\text{Mean Dia} = 41 \text{ length} = 42$$

$$1320 \times 42 \times .28 = 15,500 \#$$

$$\text{Weight of D}$$

$$1018 \times 8 \times .28 = 2,280$$

$$\text{Weight E}$$

$$13 \times 9 \times 14 \times 2 \times .28 =$$

$$\begin{array}{r} 13 \\ 14 \\ \hline 52 \\ 13 \\ \hline 182 \\ 189 \\ \hline 1638 \end{array} \quad \begin{array}{r} 1638 \\ 2 \\ \hline 3276 \\ .28 \\ \hline 26208 \\ 6552 \\ \hline 91728 \end{array}$$

$$\begin{array}{r} 28665 \\ 18 \overline{) 1949200} \\ 589 \\ 549 \\ \hline 408 \\ 408 \\ \hline 408 \\ 408 \\ \hline 320 \end{array}$$

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

SUBJECT

COMPANY

DATE

$$\text{Total weight} = 24,807$$

$$\frac{24807}{2} = 12,403$$

$$12,403 -$$

$$\frac{2590}{9803} \text{ (weight of A)}$$

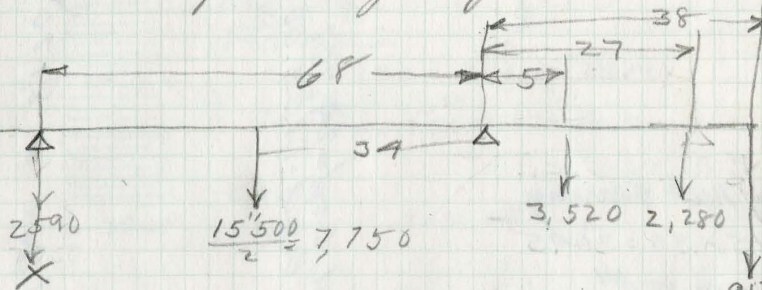
$$20 \text{ find length of B which} = 9803$$

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

$$\begin{array}{r} 21 \\ 9 \\ \hline 34 \end{array}$$



$$34 \times 15,500 + 68 \times 2590 + 68 \times =$$

$$38 \times 8,957 + 27 \times 2,280 + 5 \times 3520.$$

$$527,000 + 176,100 + 68X = 340,500 + 61,500,$$

$$+ 17600 - 340500$$

$$527000 - 61500$$

$$176100 - 17600$$

$$703,100 - 419,600$$

$$703,100 + 68X = 419,600$$

$$68X = -283,500$$

$$X = 4170 \text{ lbs.}$$

$$24807$$

$$4170$$

$$20707$$

$$8040$$

$$48240$$

$$80400$$

$$852240$$

$$100$$

$$100$$

$$100$$

$$100$$

$$\begin{array}{r} 917 \\ 206 \\ \hline 5502 \\ 18340 \\ \hline 188902 \end{array}$$

$$15500$$

$$34$$

$$62000$$

$$46500$$

$$527000$$

$$917$$

$$100$$

$$5502$$

$$9170$$

$$97202$$

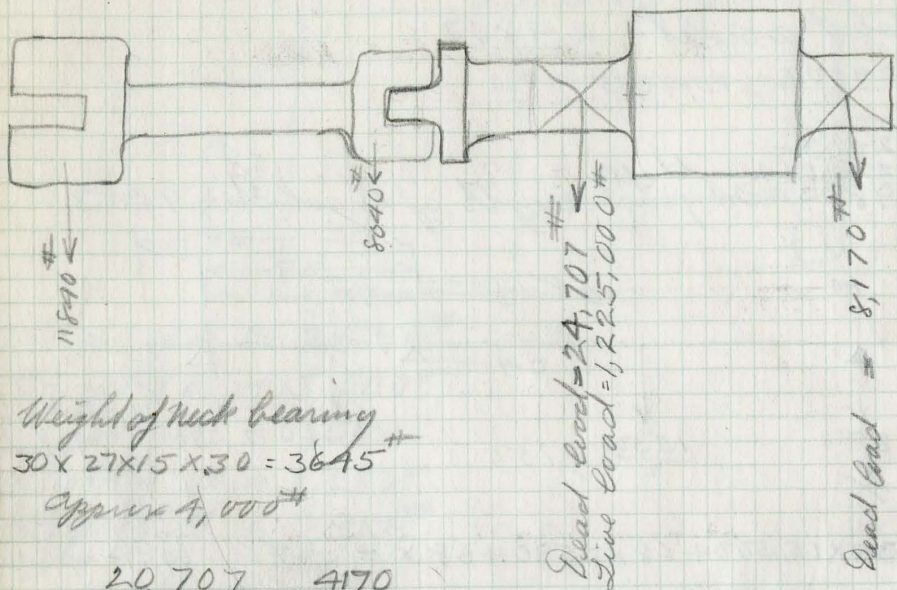
24

SUBJECT

COMPANY

Roll Loads
Jard Metals Co

DATE 12/28/23

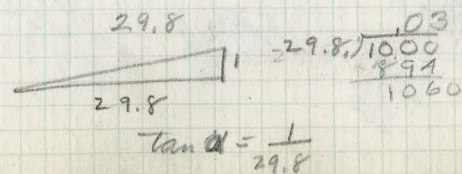


Weight of neck bearing
 $30 \times 27 \times 15 \times 30 = 3645$
 Approx 4,000

20 707	4170
4 000	21000
24 707	8170

Live Load = 1,200,000
 28,000

24 707	
3645	
28,352	
2	14,176

Pitch $L = 2$ 

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

SUBJECT

COMPANY

Adjusting Screw
Jard Metals

DATE 12/28/23

25



Mean radius = 4.75" Pitch = 1"
 Assume 3 R.P.M.

Mean dia = $9\frac{1}{2}$ " Circum = 29.8

29.8

89.4" Per min

$25,000 \times 3 = 75,000$ "Per MIN

$\frac{75,000}{12} = 6,250$ FT LBS Per min

6.250

1875.0

X = 2,500

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

$F = \frac{(25,000)(4.75)(.3 + .0336)}{12 \text{ (avg) lever arm}}$

$F = \frac{(188,000)(.3336)}{12}$

$F = \frac{62,700}{12}$

$F = 5,220$

$18.8 \times 5,220 = 93,300$ lbs per min

25,000

75,000

37,500

$37,500$ lbs

$K = \frac{r}{V_L} = \frac{4.5}{1.41} = 3.2$

$(3)(2\pi 3.2) = \frac{60.5}{12} = 5 \text{ ft}$

93300

37500

130800

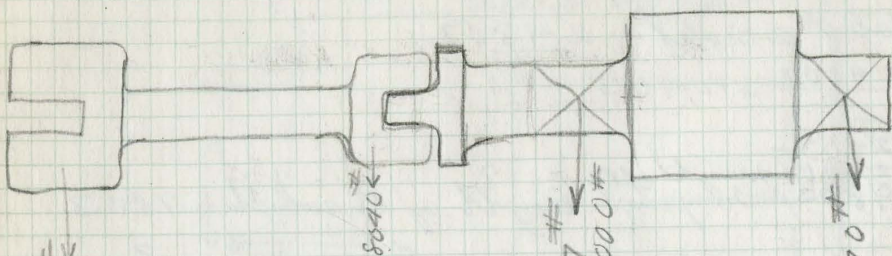
$\frac{130,800}{33,000} = 4.18$ H.P.

4.18 HP Required to raise screw
 3" in 1 minute

See P 27

SUBJECT Roll Loads
 COMPANY Lord Motors Co

DATE 12/28/23



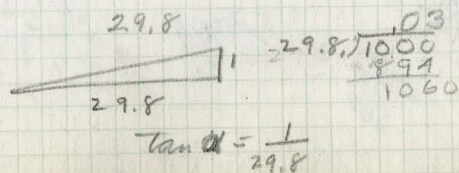
Weight of neck bearing
 $30 \times 27 \times 15 \times 30 = 3645$
 Approx 4,000#

20 707	4170
4 000	4000
24 707	8170

Live Load = $\frac{1,200,000}{25,000}$

24 707	
3645	
28,352	
2	14,176

Pitch $L = 2$



$$\tan \alpha = \frac{1}{29.8}$$

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

SUBJECT Adjusting Screw
 COMPANY Lord Motors

DATE 12/28/23



Mean radius = 4.75" Pitch = 1"
 Assume 3 R.P.M.

Mean dia = $9\frac{1}{2}$ " Circum = 29.8

29.8

89.4" Per min

$25,000 \times 3 = 75,000$ " Per MIN

$\frac{75,000}{12} = 6,250$ FT LBS Per min

6,250

1875.0

X = 2,500

WORCESTER, MASS.

CO.

PROPERTY OF MORGAN CONSTRUCTION

$$F = \frac{(25,000)(4.75)(.3 + .0336)}{12 \text{ (avg) lever arm}}$$

$$F = \frac{(188,000)(.3336)}{12}$$

$$F = \frac{62,700}{12}$$

$$F = 5,220 \text{#}$$

$$18.8 \times 5,220 = 93,300 \text{ lbs per min}$$

$$\frac{25,000}{75,000} = .333$$

$$\frac{37,500}{60} = 625 \text{ lbs}$$

$$K = \frac{r}{V_L} = \frac{4.5}{1.41} = 3.2$$

$$(3)(2\pi 3.2) = \frac{60.5}{12} = 5 \text{ ft}$$

$$\frac{93,300}{1,308,000} = .071$$

$$\frac{130,800}{33,000} = 4.18 \text{ H.P.}$$

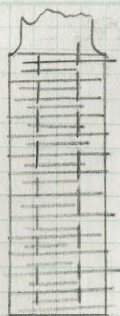
4.18 HP Required to raise screw
 3" in 1 minute

See P 27

SUBJECT

COMPANY

DATE



Adj Screw shaft,

to transmit 10 HP at 3 R.P.M. Absorbs 7,000

$$d = \sqrt[3]{\frac{321,000(10)}{(3)(7000)}}$$

$$d = \sqrt[3]{\frac{3,210,000}{21,000}} = \sqrt[3]{153}$$

$$d = 5.34"$$

130,800 ft. lbs. per min

18.9 ft per min 7300 lbs

7,300 lbs at end of 12" lever arm.

$$P \times R = S \times Z \times p$$

$$7300 \times 12 = 7000 \times .08 d^3$$

$$87,500 = 560 d^3$$

$$d^3 = \frac{87500}{560} = 157$$

$$d = 5\frac{1}{2}" = \text{cor to cor of sq shaft}$$

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SUBJECT

COMPANY

DATE

See Mark P292

$$\frac{122,500}{63}$$

$$63 \overline{) 122500} \\ \underline{63} \\ 595 \\ \underline{567} \\ 28$$

$$M = \frac{1}{2} f L D$$

$$M = \frac{1}{2} (.3)(24,707)(9)$$

$$222,200 \times .3$$

$$\frac{66,660.0}{2} = 33,330$$

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$$M = 33,330$$

$$2\pi MN = \text{work expended in in lbs.} \\ (18.85)(33,330)$$

$$628,000 \text{ inch lbs per min}$$

$$\frac{52300}{33,000} \text{ ft lbs per min}$$

$$33,000$$

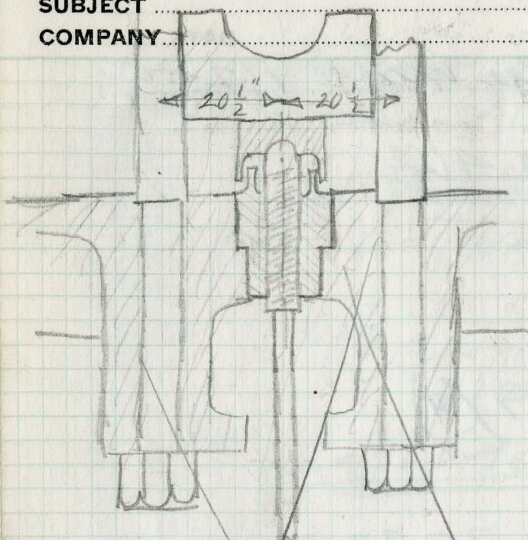
$$= 1.58 \text{ H.P. absorbed by hemispherical Pivot}$$

$$\begin{array}{r} 63.5 \\ 28.25 \\ \hline 35.25 \end{array}$$

SUBJECT

COMPANY

DATE

Pin load
= 1,225,000Max bending moment $\frac{W L}{4}$

$$(1,225,000)(41)$$

$$\frac{50,225,000}{4}$$

$$= 12,556,250 \text{ in.}^2 \text{ B.M.}$$

$$\frac{12,556,250}{2000} = 6278$$

$$I = 6278 = \frac{b h^3}{12} = \frac{(18)(110592)}{12} = 1990658$$

$$I = 166000$$

$$48 \times 18 = 864 \text{ in.}^2$$

See Page 31

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$$\begin{array}{r} 110592 \\ 18 \\ \hline 884738 \end{array}$$

$$\begin{array}{r} 1990658 \\ 18 \\ \hline 884738 \end{array}$$

SUBJECT

COMPANY

DATE

Top Roll Supporting Pins

$$\text{Load on each pin} = \frac{28352}{2} = 14,176 \text{ lbs}$$

Assuming pins $1\frac{1}{2}$ " dia. Then find
compression per sq inch = 8,000 lbs/sq in.

$$A^2 = 5620 \text{ in.}^2 = 1.77 \text{ sq in.}$$

$$\frac{14,176}{1.77} = 8,000 \text{ lbs}$$

Ratio of slenderness

36" = length

$$\text{Radius of gyration} = K = \frac{R}{\sqrt{2}} = \frac{.75}{1.41} = .53 \text{ in.}$$

$$\frac{36}{.53} = 68$$

$$P = \frac{50,000}{C^2} = \frac{50,000}{1 + \frac{1,116}{18,000}} = \frac{50,000}{1.062}$$

$$= 30800 \text{ lbs}$$

$$\frac{30,800 \times 3.14}{6} = \frac{96800}{6} = 12,800$$

safe load per sq in 12,800 lbs

actual load per sq in 8,000 lbs

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SUBJECT

COMPANY

Sack Motor Co

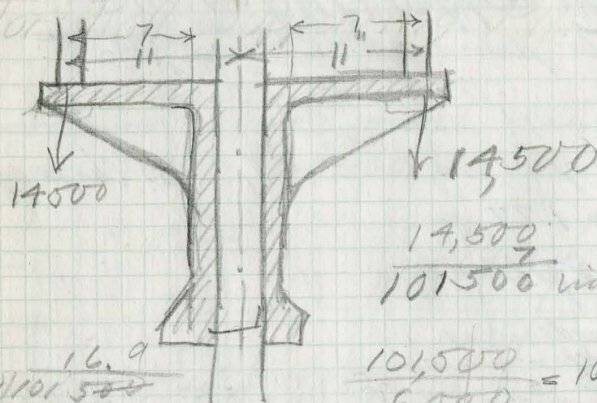
DATE

11/1/24

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$$\frac{14,500}{101,500} \text{ inch lbs.}$$

$$\frac{10,500}{6,000} = 16.9$$

$$\frac{f}{c} = 16.9$$

$$\frac{bh^2}{6} = \frac{b \cdot 16}{6} = 16.9$$

$$b \cdot 16 = 101.4$$

$$b =$$

$$b \cdot 25 = 101.4$$

$$b = 4$$

$$\begin{array}{r} 1240000 \\ 41 \\ \hline 1240000 \\ 4960000 \\ \hline 50840000 \end{array}$$

8473

$$1500 / 12710000$$

$$12000$$

$$7100$$

$$6000$$

$$11000$$

$$10500$$

$$5000$$

$$\begin{array}{r} 220 \\ 2304 / 50838 \\ \hline 9668 \\ 4858 \\ 4608 \\ \hline 2500 \end{array}$$

$$\begin{array}{r} 2304 / 38130 \\ \hline 2304 \\ \hline 15090 \\ 13824 \\ \hline 12660 \end{array}$$

$$\begin{array}{r} 2304 \\ 6 \\ \hline 13824 \end{array}$$

SUBJECT

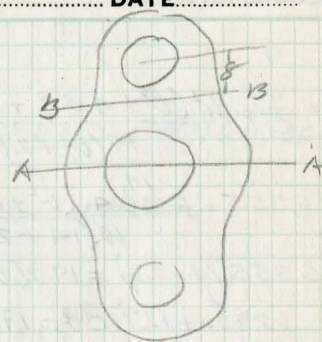
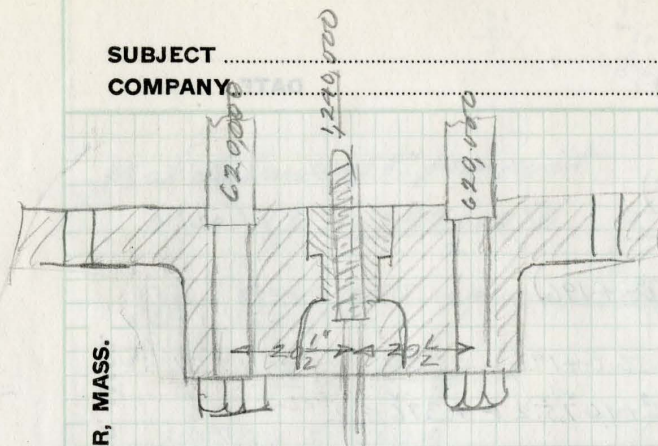
COMPANY

DATE

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$$\text{Max bending moment} = PL$$

$$M = \frac{(1,240,000)(41)}{4} = \frac{50,840,000}{4}$$

$$M = 12,710,000 \text{ inch lbs.}$$

$$\frac{I}{C} = \frac{12,710,000}{1,500} = 8473 \text{ section modulus}$$

$$\frac{I}{C} = \frac{bh^2}{6} = \frac{b \cdot 16}{6} = 8473 \text{ section modulus}$$

$$8473 = \frac{b \cdot 2304}{6}$$

$$2304b = 50838$$

$$b = 22$$

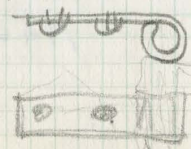
$$\frac{I}{C} = \frac{12,710,000}{2000} = 6,355 \text{ section modulus}$$

$$6,355 = \frac{b \cdot 2304}{6}$$

$$2304b = 38130$$

$$b = 16.5$$

$$\text{stressed to } 2000 \text{ psi}$$



SUBJECT

COMPANY

DATE

$$\frac{I}{C} = \frac{1.4(b^3 + 4bh^2 + h^3)}{12(b + 2h)}$$

$$6,355 = \frac{1.4}{12} (b^3 + 56b + 196)$$

$$6,355(14 + 2b) = 19.2(b^3 + 56b + 196)$$

$$88,970 + 127,108b = 19.2b^3 + 1,075.2b + 3,763.2$$

$$-19.2b^3 + 116,355b + 85,207 = 0$$

$$X = -116,355 \pm \sqrt{135,378,225 + 6,543,896}$$

$$-38.4$$

$$X = -116,355 \pm \sqrt{141,922,121}$$

$$-38.4$$

$$X = -116,355 \pm 11,913$$

$$-38.4$$

$$38.4X = 116,355 \pm 11,913$$

$$38.4X = 235,48$$

$$X = 613$$

$$X = 7.2$$

$$\frac{1,240,000}{9,920,000}$$

$$\frac{2,486}{14,960,000}$$

$$\frac{4,000}{9600}$$

$$\frac{8000}{16000}$$

$$\frac{16000}{16000}$$

$$141,922,121 / 11,913$$

$$\begin{array}{r} 21 \overline{) 41} \\ 21 \\ \hline 229 \overline{) 2092} \\ 2061 \\ \hline 2381 \overline{) 3121} \\ 2381 \\ \hline 23823 \overline{) 71469} \end{array}$$

196

$$\begin{array}{r} 19.2 \\ 6355 \\ \hline 25420 \\ 6355 \\ \hline 88970 \end{array}$$

$$\begin{array}{r} 196 \\ 19.2 \\ \hline 392 \\ 1764 \\ 196 \\ \hline 3763.2 \end{array}$$

$$\begin{array}{r} 12710 \\ 1075 \\ \hline 11635 \end{array}$$

$$\begin{array}{r} 88970 \\ 3763 \\ \hline 85207 \end{array}$$

$$\begin{array}{r} 11635 \\ 11913 \\ \hline 23548 \\ 11913 \\ \hline 11635 \\ 278 \end{array}$$

$$\begin{array}{r} 11635 \\ 11635 \\ \hline 23548 \\ 34905 \\ \hline 69810 \\ 11635 \\ \hline 11635 \\ 135,378,225 \end{array}$$

$$\begin{array}{r} 85207 \\ 19.2 \\ \hline 170414 \\ 766863 \\ 85207 \\ \hline 1635974.7 \\ 4 \\ \hline 6,543,896 \end{array}$$

$$\begin{array}{r} 19.2 \\ 2 \\ \hline 38.4 \end{array}$$

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$$\begin{array}{r} 23823 \\ 3 \\ \hline 71469 \end{array}$$

SUBJECT

COMPANY

DATE 1/2/27

Mat distance of 8" from post

$$M_x = \frac{WX}{2} = \frac{(1,240,000)(8)}{2} = \frac{9,920,000}{2} = 4,960,000$$

$$\frac{I}{C} = \frac{4,960,000}{2,000} = 2,480 = \text{section modulus}$$

$$\frac{I}{C} = \frac{bh^2}{6} = \frac{b \cdot 2304}{6}$$

$$2480 = \frac{b \cdot 2304}{6}$$

$$2304b = 14880$$

$$b = 6.5$$

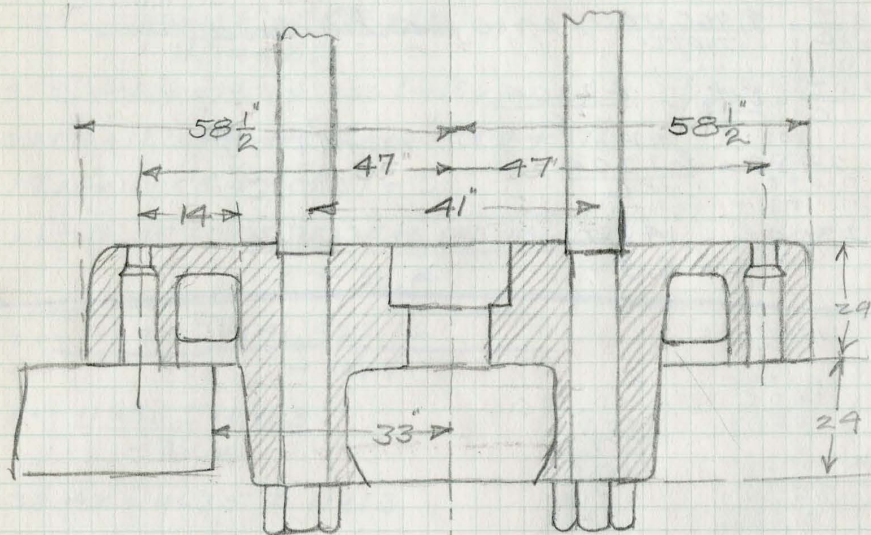
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SUBJECT

COMPANY *Ind. Motor Co.*DATE *1/3/23*

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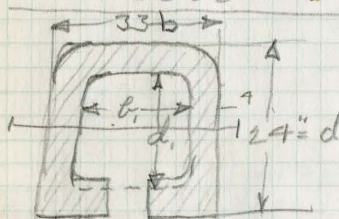
$$T.N. 4 \text{ Bolt} = 99700 \quad \begin{matrix} 47 \\ 33 \end{matrix}$$

$$99700$$

$$199,400$$

$$199,400 \times 14 = 2,791,600 \text{ inch}$$

$$\frac{2,791,600}{2000} = 1,395.8 = \frac{I}{C} \text{ section modulus}$$



$$S = \frac{bd^3}{12} - \frac{b_1d_1^3}{12}$$

$$S = \frac{33 \times 13824}{144} - \frac{(25) \times (4096)}{144}$$

$$S = \frac{445,192 - 102,400}{144}$$

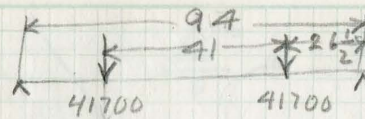
$$S = \frac{342,792}{144}$$

$$S = 2,380$$

$$\begin{array}{r} 29 \\ 6 \\ 144 \\ \hline 13824 \\ 33 \\ \hline 40472 \\ 40472 \\ \hline 445,192 \\ 1728 \\ 25 \\ \hline 8640 \\ 3456 \\ \hline 43200 \\ 445192 \\ 43200 \\ \hline 401992 \end{array}$$

SUBJECT

COMPANY

DATE *1/3/23*Weight of guides per strand *8,000*

$$\begin{array}{r} 32 \\ \text{caps} = 25000 \\ 1 \text{ lock nut} = 4800 \\ \text{cap cover} = 6500 \\ 1 \text{ post} = 33200 \\ \text{end cover} = 3000 \\ \text{neck bearings} = 14600 \\ \text{Bolt} = 30000 \\ \text{Rolls} = 49200 \\ \hline 166800 \end{array}$$

83,400

$$M = W \times L$$

$$M = 41700 \times 26 \frac{1}{2}$$

$$M = 1,105,000 \text{ inch}$$

$$S = \frac{1,105,000}{2000} = 552$$

$$\frac{83,400}{2} = 41,700$$

$$\begin{array}{r} 41700 \\ 26.5 \\ \hline 208500 \\ 250200 \\ 83400 \\ \hline 1,105,000 \end{array}$$

$$\text{Pal Modulus} = 6,907$$

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$$\begin{array}{r} 4096 \\ 25 \\ \hline 20480 \\ 8192 \\ \hline 102400 \end{array}$$

$$\begin{array}{r} 445192 \\ 102400 \\ \hline 342792 \end{array}$$

$$\begin{array}{r} 28665 \\ 2 \\ \hline 57330 \end{array}$$

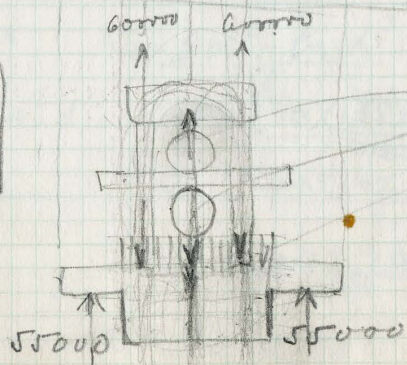
SUBJECT
 COMPANY DATE

50,000

600,000 → 560,000
 35,000
 15,000

600,000 → 560,000
 25,000
 15,000

1200,000
 300,000
 1,500,000



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 COMPANY DATE

~~$$\frac{5h^2}{6} = 9m \text{ Tm}$$~~

~~$$32 \times 48^2 - (18 \times 10^2 + 18.5 \times 10^2 + 16 \times 3^2 - 12 \times 25^2)$$~~

~~$$32 \times 2304 = 73600$$~~

1810 +
 1350
 144
 7500

~~$$18 \times 400 = 72000$$~~

18000
 72000
 90000 3600
 25

~~$$14 \times 13^3$$~~

2200
 2800
 2800
 30800

~~$$15000 \times 1500$$~~

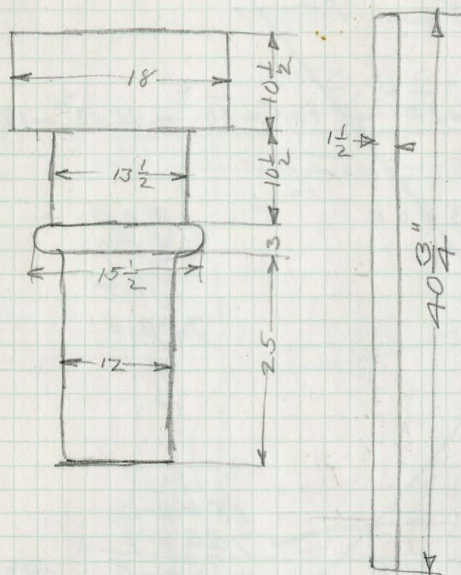
15000
 1500
 12 72000
 73800 3290
 25

~~$$32.5 \times 48^2 - 13.5 \times 48^2$$~~

~~$$\frac{19 \times 48^2}{6} = \frac{43800}{6} = 7300$$~~

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SUBJECT
 COMPANY DATE



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SUBJECT *Much of Best*
 COMPANY *Shelton Co.* DATE

804.25
 210
 594.25
 196.5
 791.75

17.
 283.5
 87
 196.5

$$791 \times 48 = 380180$$



40
 49 1/2
 36
 60 1/2
 12
 198 1/2
 46
 1188
 792
 9108

16 1/2
 3
 48 1/2

24
 24
 96
 48
 576
 18
 4608
 576
 10368
 9
 41472

38018
 9108
 47126
 2
 94252
 41472
 135722

135722 cu in.

40716.6

40716 #

20 tons

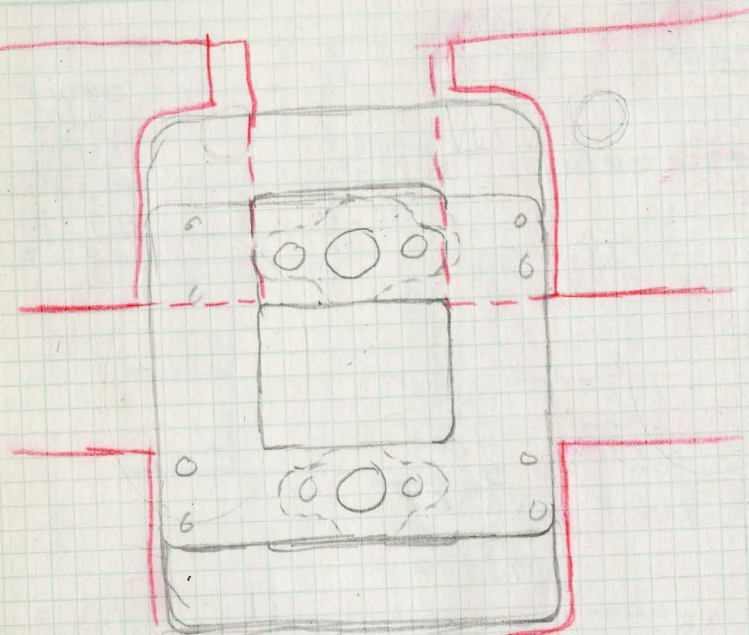
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SUBJECT
 COMPANY DATE



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SUBJECT
 COMPANY DATE

10 H.P.

72" Circum

18 feet per min

330,000 = 10 HP Per Min

18,300# = Tooth Pressure

W = spfy

$$18,000 = (8,500)(1.5)(.112)(7)$$

12,000

$$18,000 = \$1345$$

14.9

11,000 / 44.7

49,000" #

40,900 # lbs

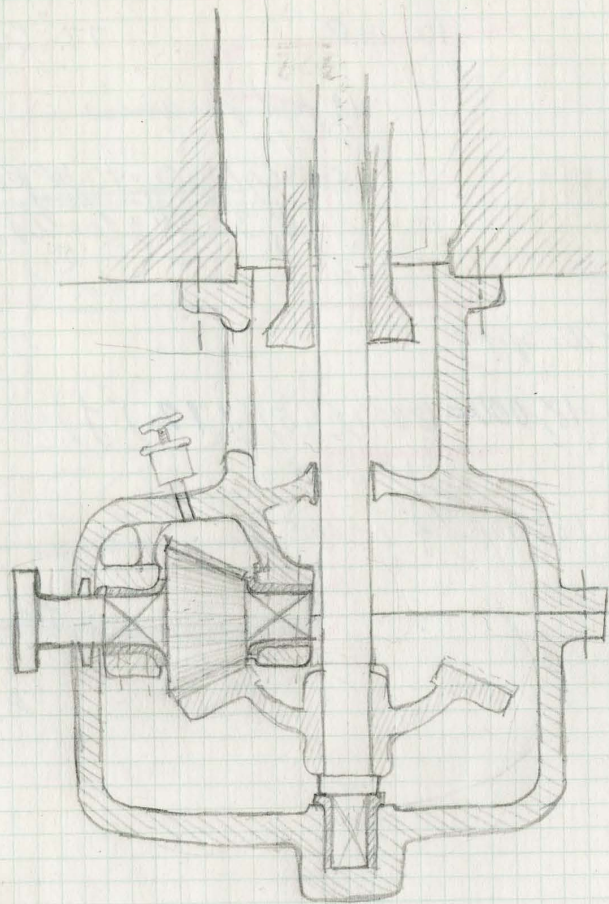
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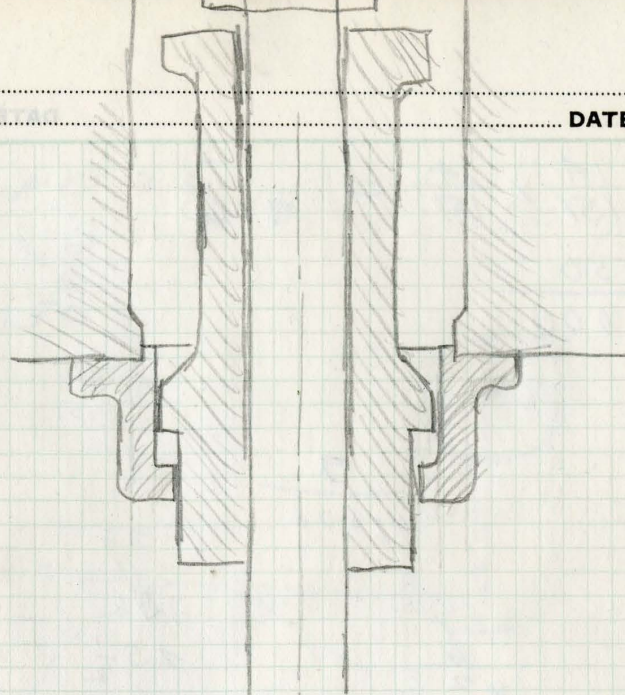
SUBJECT
COMPANY DATE



PROPERTY OF MORGAN CONSTRUCTION CO. WORCESTER, MASS.

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SUBJECT
COMPANY DATE



PROPERTY OF MORGAN CONSTRUCTION CO. WORCESTER, MASS.

SUBJECT
 COMPANY DATE

$$\frac{13}{40} \times \frac{14}{151} \times \frac{14}{151} = \frac{1}{376}$$

$$\frac{2550}{912,000}$$

$$\frac{27}{6} = 162$$

$$\frac{9}{11,000}$$

154

$$\begin{array}{r} 26 \\ 6 \\ \hline 156 \\ 25\frac{1}{2} \\ 6 \\ \hline 150 \\ 3 \\ \hline 153 \end{array}$$

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SUBJECT
 COMPANY DATE

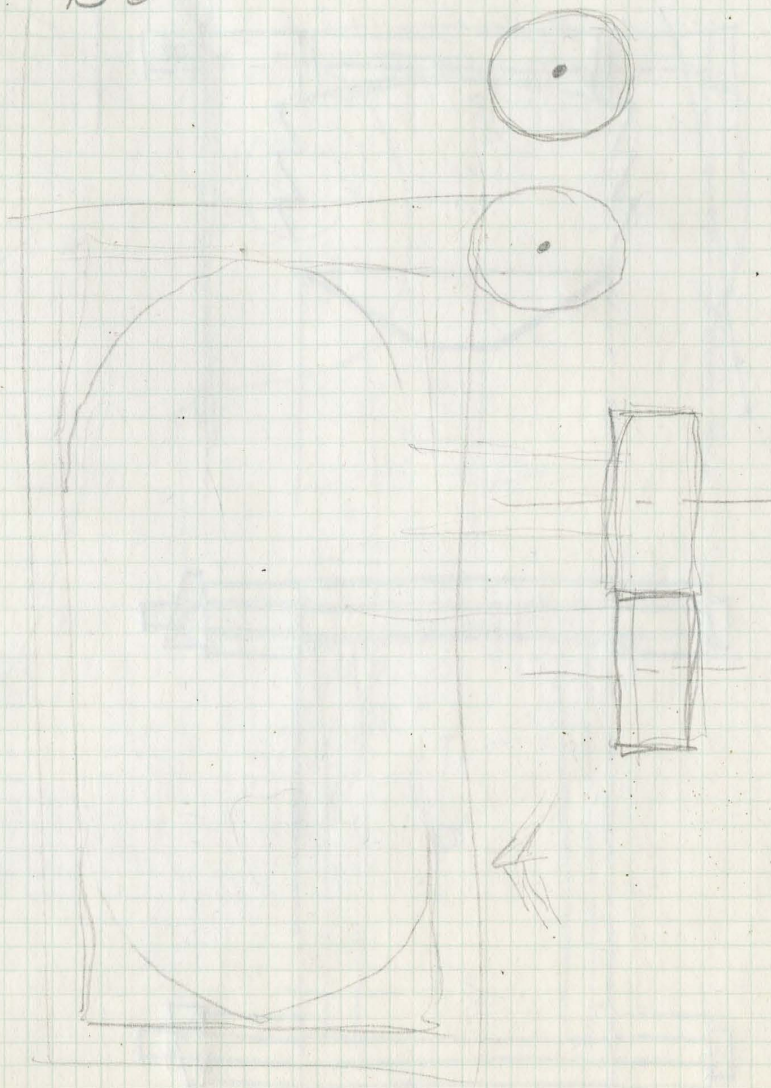
P17 25

$$\frac{29}{150}$$

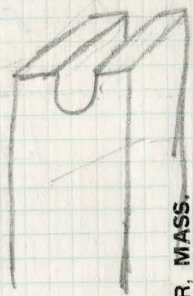
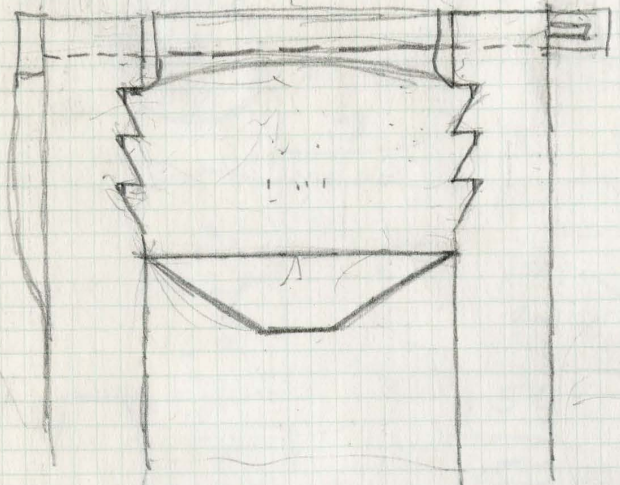
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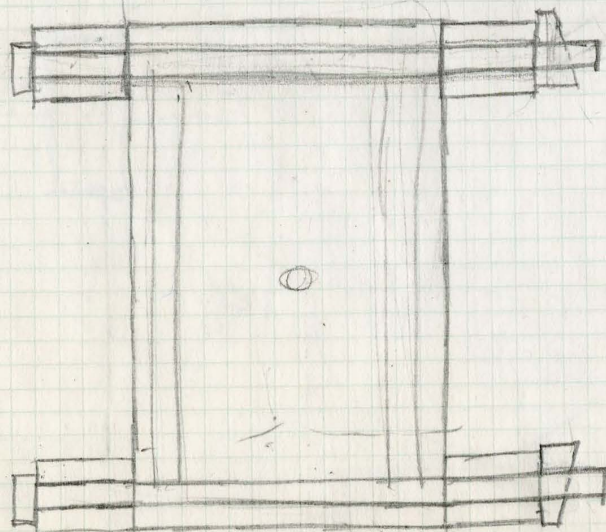
SUBJECT
COMPANY DATE 7/11/92



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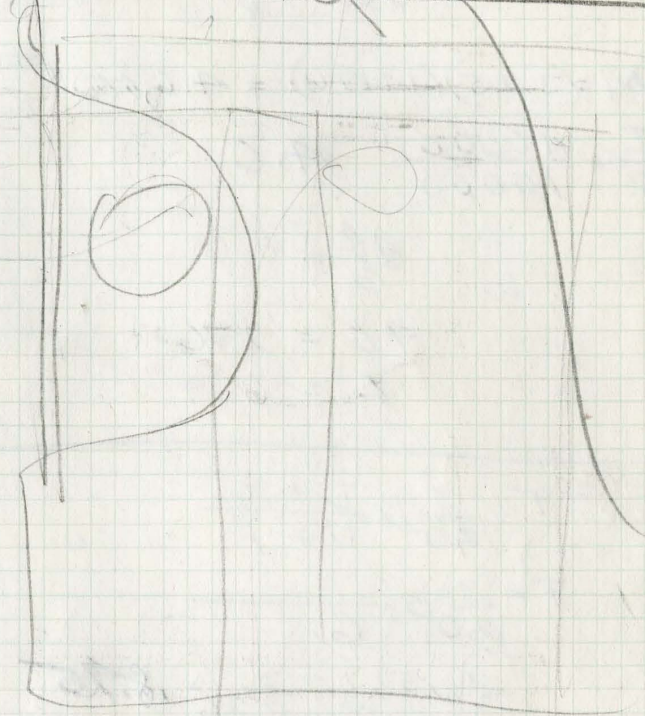
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SUBJECT
COMPANY DATE

Add Notes on Drug A33121



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SUBJECT _____
 COMPANY _____ DATE _____

14176
 ↓
 3.25

for shear $\frac{14176}{10,000} = 1.4176$

$$M = (3.25)(14176) = 46,000 \text{ " \#}$$

$$\frac{I}{C} = \frac{46000}{10000} = 4.6$$

$$\frac{46}{6} = 7.6$$

$$7.6 = 27.6$$

$$L = 6.9$$

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$$T = \frac{3}{20} \frac{D+2}{D+1}$$

4

$$T = \frac{3}{20} \left(\frac{5}{6} \right) \left(\frac{7}{6} \right)$$

$$\frac{3}{20} \times \frac{5}{6} \times \frac{7}{6} = \frac{35}{40} = 0.875$$

